

FOAM REPLICATED POROUS 316L STAINLESS STEEL BASED ON TAGUCHI
METHOD FOR BIOMEDICAL APPLICATIONS

FAZIMAH BINTI MAT NOOR

A thesis submitted in fulfilment of the
requirements for the award of the degree of
Doctor of Philosophy



Razak School of UTM in Engineering and Advanced Technology
Universiti Teknologi Malaysia

June 2018

“My dearest mum, family, and friends”

This is for all of you



PTTA UTHM
PERPUSTAKAAN TUNKU TUN AMINAH

ACKNOWLEDGEMENT

First and foremost, I would like to express my gratitude to my supervisor, Associate Professor Dr. Khairur Rijal Jamaludin and my co-supervisor, Associate Professor Dr. Sufizar Ahmad for giving me the opportunity to work on an interesting topic that inspired passion in me, and for encouraging and advising me throughout the past few years. I have learned a lot from them especially about creative and critical thinking, and self-motivation in researching. Their trust, understanding, and consideration have been invaluable and are highly appreciated. I will strive to carry these qualities with me in the future.

My sincere thanks also goes to Dr. Rosdi and Mr. Nizam from Advanced Materials Research Centre (AMREC), SIRIM Bhd. for their help with the vacuum furnace. Thank you to everyone who helped me with my work. Thank you to all my friends for always filling the work place with fun and happiness, as well as offering great help in every way. It has been such a wonderful journey and great pleasure working with all of you. I also would like to acknowledge support from Malaysian Ministry of Higher Education through the research funding (ERGS-E028) and for the PhD scholarship.

Above all, I would like to give my special thanks to my family: my mom, my husband and my daughters for giving me this life full with love and happiness, for being a driving forces in my life, and for positive support in all direction.

ABSTRACT

The mismatch between elastic modulus of metal implants and bones which is also known as stress shielding, remains an unresolved issue. Porous metals are one of the most effective ways of reducing stiffness mismatches and achieving stable long-term fixation via full bone in-growth. In this work, porous SS316L is produced using the foam replication technique. The samples were each produced with different compositions of SS316L powders and sintered at various sintering parameters including the sintering temperature, sintering time, heating rate and cooling rate. Scanning electron microscopy (SEM) was used to characterise the microstructure while a compression test was used to determine the mechanical properties of the samples. The physical properties including porosity and density were measured according to the Archimedes principles. The biocompatibility test showed that the porous SS316L produced, exhibited no cytotoxicity reactivity. Furthermore, the optimisations of the sintering parameters were performed using the Taguchi method. The optimised porosity of porous SS316L prepared by ball milling method was 85.44% and achieved using sintering time of 60 minutes, sintering temperature of 1200°C, heating rate of 1°C/min, SS316L composition of 60 wt% and cooling rate of 1°C/min. Whereas, for samples prepared by mechanical stirring method, the optimum porosity was 79.46% and occurred for the samples sintered within 60 minutes at 1200°C of sintering temperature, with the cooling and heating rates of 1°C/min and 2°C/min respectively, and prepared with 70 wt% of SS316L composition. In addition, porous SS316L prepared by ball milling method with modulus of elasticity of 0.08 GPa was obtained by using optimum sintering temperature of 1250°C, sintering time of 60 minutes, heating rate of 2°C/min, SS316L composition of 65 wt% and cooling rate of 1°C/min. Whereas, the modulus of elasticity of 0.05 GPa for porous SS316L prepared by mechanical stirring method was obtained by using the optimum cooling rate of 5°C/min, sintering temperature of 1200°C, sintering time of 120 minutes, SS316L composition of 70 wt% and heating rate of 0.5°C/min respectively. Following optimisation, the porous SS316L produced was found to have attractive mechanical and physical properties much like human bone. Notwithstanding, this included interconnected and open porosity in the range of 79.46 to 85.44 %, density in the range of 1.53-1.76 g/cm³, pore size in the range of 247–470 µm, modulus of elasticity in the range of 0.05-0.08 GPa, yield strength in the range of 0.52–0.82 MPa and compression strength in the range of 35.87-64.43 MPa.

ABSTRAK

Perbezaan modulus elastik antara bahan implan dan tulang yang juga dikenali sebagai kesan perisai tegasan merupakan masalah yang masih belum selesai. Logam berbusa adalah salah satu pendekatan yang berkesan untuk menangani masalah ini supaya ia sesuai untuk aplikasi jangka panjang melalui pertumbuhan tulang sepenuhnya. Dalam kajian ini, SS316L berbusa telah dihasilkan dengan menggunakan teknik replikasi Poliurethana (PU) berbusa. Sampel dihasilkan dengan komposisi serbuk SS316L yang berbeza, dan disinter pada pelbagai parameter persinteran termasuk suhu persinteran, masa persinteran, kadar pemanasan dan kadar penyejukan. Pengimbasan mikroskop elektron (SEM) digunakan untuk mengkaji mikrostruktur manakala ujian mampatan dijalankan untuk menentukan sifat-sifat mekanik sampel. Ciri-ciri fizikal iaitu keliangan dan ketumpatan diukur menggunakan prinsip Archimedes. Ujian biokompatibiliti telah menunjukkan bahawa SS316L berbusa yang dihasilkan tidak menunjukkan reaktiviti sitotoksik. Selain itu, pengoptimuman parameter persinteran dilakukan dengan menggunakan kaedah Taguchi. Keliangan optimum untuk SS316L berbusa yang disediakan dengan kaedah pengisaran bebola adalah 85.44% dan diperoleh dengan menggunakan masa persinteran selama 60 minit pada suhu 1200°C dengan kadar pemanasan 1°C/min, disediakan dengan komposisi SS316L sebanyak 60 wt% serta disejukkan dengan kadar penyejukan pada 1°C/min. Manakala untuk sampel yang disediakan dengan kaedah pengadukan mekanikal, keliangan optimum adalah 79.46% dan dicapai setelah disinter selama 60 minit pada suhu 1200°C, dengan kadar penyejukan dan pemanasan masing-masing pada 1°C/min dan 2°C/min, dan disediakan dengan komposisi SS316L sebanyak 70 wt%. Di samping itu, SS316L berbusa yang disediakan dengan kaedah pengisaran bebola dengan modulus keanjalan optimum, 0.08 GPa diperoleh dengan menggunakan suhu persinteran pada 1250°C, masa persinteran selama 60 minit, kadar pemanasan pada 2°C/min, komposisi SS316L sebanyak 65 wt% dan dengan kadar penyejukan pada 1°C/min. Manakala modulus keanjalan optimum, 0.05 GPa untuk SS316L berbusa yang disediakan oleh kaedah pengadukan mekanikal pula diperoleh dengan menggunakan kadar penyejukan optimum pada 5°C/min, suhu persinteran pada 1200°C, masa persinteran selama 120 minit, komposisi SS316L sebanyak 70 wt% dan kadar pemanasan pada 0.5°C/min. Selepas pengoptimuman, SS316L berbusa yang dihasilkan didapati mempunyai sifat mekanikal dan fizikal yang hampir sama dengan tulang manusia. Walau bagaimanapun ini termasuk keliangan terbuka yang saling berkait dalam lingkungan 79.46-85.44%, ketumpatan di antara 1.53 -1.76 g/cm³, saiz liang di antara 247-470 µm, modulus keanjalan di antara 0.05-0.08 GPa, kekuatan alah di antara 0.52-0.82 MPa dan kekuatan mampatan dalam lingkungan 35.87-64.43 MPa.

TABLE OF CONTENT

CHAPTER	TITLE	PAGE
	DECLARATION	ii
	DEDICATION	iii
	ACKNOWLEDGEMENTS	iv
	ABSTRACT	v
	ABSTRAK	vi
	TABLE OF CONTENTS	vii
	LIST OF TABLES	x
	LIST OF FIGURES	xiii
	LIST OF ABBREVIATIONS	xix
	LIST OF SYMBOLS	xx
	LIST OF APPENDICES	xxii
1	INTRODUCTION	1
	1.1 Research Background	1
	1.2 Problem Statement	3
	1.3 Research Objectives	5
	1.4 Scopes of study	6
	1.5 Significance of Research	6
	1.6 Thesis Outline	7
2	LITERATURE REVIEW	9
	2.1 Introduction to biomedical implant	9
	2.2 Characteristics and Properties of Natural Bone	10
	2.3 Porous Materials for Biomedical Implant	13

2.4	Porous Metal for Biomedical Implant	17
2.5	Fabrication of Porous Materials	21
2.6	Foam Replication Method	22
2.7	Stainless Steel for Biomedical Implants	28
2.8	Sintering of metal foams	37
2.9	Taguchi Method	47
2.10	Chapter summary	50
3	METHODOLOGY	52
3.1	Introduction	52
3.2	Materials	52
3.3	Preparation of Porous SS316L	55
3.4	Characterization of the Samples	61
3.4.1	Thermal Gravimetric Analysis	61
3.4.2	Scanning Electron Microscope (SEM)	62
3.4.3	Energy Dispersion X-Ray (EDX)	63
3.4.4	Shrinkage	63
3.4.5	Density and Porosity Test	64
3.4.6	Compression Test	65
3.5	Biocompatibility Test	67
3.5.1	In-Vitro Test	67
3.5.2	Cytotoxicity Test	69
3.6	Taguchi Robust Parameter Design	70
4	RESULTS AND DISCUSSIONS	75
4.1	Development of porous SS316L by using foam replication method	75
4.1.1	Effects of Binder and SS316L Composition on the Microstructure	79
4.1.2	Effects of Sintering Temperature on the Microstructure of Porous SS316L	88
4.2	Physical Properties of Porous SS316L	92
4.3	Mechanical Properties of Porous SS316L	94
4.4	Biocompatibility of Porous SS316L	96

4.4.1	Assessment of Cytotoxicity of Porous SS316L	96
4.4.2	Assessment of Bioactivity of Porous SS316L	99
4.5	Optimization of Sintering Parameters by Using Taguchi Method	101
4.5.1	Optimisation of Shrinkage Percentage	102
4.5.2	Optimisation of Porous SS316L Density	110
4.5.3	Optimisation of Porous SS316L Porosity	116
4.5.4	Optimisation of Porous SS316L Modulus of Elasticity	122
4.5.5	Optimisation of Porous SS316L Yield Strength	128
4.5.6	Optimisation of Porous SS316L Compression Strength	134
4.6	Microstructural Analysis of Porous SS316L produced for Optimization	140
5	CONCLUSIONS AND RECOMMENDATIONS	146
5.1	Conclusions	146
5.2	Contributions	150
5.3	Recommendations	151
	REFERENCES	153
	Appendices A-B	168-175

LIST OF TABLES

TABLE NO.	TITLE	PAGE
2.1	Mechanical and physical properties of natural bone	12
2.2	Metals implant and implant division	19
2.3	Advantages and disadvantages of metallic materials for orthopaedic applications	21
2.4	Effects of binder types and compositions on the Slurry's properties	25
2.5	Microstructure and properties of porous Materials prepared by foam replication method.	26
2.6	Stainless steel foam developed by various fabrication methods	36
2.7	Sintering parameters	39
2.8	Mechanical properties of porous 316L stainless steel sintered at different temperatures.	43
2.9	Sintering parameters of stainless steel by previous work	45
2.10	L9 orthogonal array for the experimental layout and factors distribution	49
2.11	Experimental layout using L9 orthogonal array	50
3.1	Properties of SS316L	53
3.2	As received SS316L powder	54
3.3	Specification of PEG (10000)	54
3.4	Specification of CMC	54
3.5	Porous SS316L compositions	55
3.6	Amount of each reagent for SBF preparation by T. Kokubo	68
3.7	Control factors and level	72

3.8	Orthogonal array L18 for the optimization of the sintering parameters	72
3.9	S/N Ratio for Static Problems	73
4.1	Parameters for the trial and error experiment.	76
4.2	Microstructure of the porous SS316L with 40 wt%, 50 wt% and 60 wt% SS316L compositions produced in the fifth trial	82
4.3	Microstructure of the porous SS316L with 60 wt%, 65 wt% and 70 wt% SS316L compositions produced in the sixth trial	86
4.4	Composition of porous SS316L determined by EDX	88
4.5	SEM images of porous SS316L sintered at (a) 1200°C, (b) 1250°C, and (c) 1300°C	90
4.6	Composition of porous SS316L determined by EDX	91
4.7	Qualitative cytotoxicity grade	96
4.8	Conditions of cultures before and after treatment.	97
4.9	Summary of cytotoxicity grading on cultures.	98
4.10	S/N ratio, variance and mean response for shrinkage percentage.	103
4.11	The optimum parameters for shrinkage percentage of porous SS316L	106
4.12	The confirmation result for shrinkage percentage of porous SS316L	107
4.13	Comparison between the S/N ratio of porous SS316L shrinkage percentage before and after optimization	107
4.14	S/N ratio, variance and mean response for the porous SS316L density	110
4.15	Optimum parameters for the density of porous SS316L	112
4.16	The confirmation result of porous SS316L density	112
4.17	Comparison between the S/N ratio of porous SS316L Density before and after optimization	113
4.18	S/N ratio, variance and mean response for porosity	116
4.19	The optimum parameters for the porosity of porous SS316L	118
4.20	The confirmation result of porous SS316L porosity	118

4.21	Comparison between the S/N ratio of porous SS316L porosity before and after before optimisation	119
4.22	S/N ratio, variance and mean response for modulus of elasticity	122
4.23	The optimum parameters for the modulus of elasticity of porous SS316L.	124
4.24	The confirmation result of the porous SS316L modulus of elasticity	125
4.25	Comparison between the S/N ratio of porous SS316L modulus of elasticity before and after optimisation	125
4.26	S/N ratio, variance and mean response for yield strength	128
4.27	The optimum parameters for for the yield strength of porous SS316L	131
4.28	The confirmation result of porous SS316L yield strength	131
4.29	Comparison between the S/N ratio of porous SS316L yield strength before and after optimisation	131
4.30	S/N ratio, variance and mean response for compression strength	134
4.31	The optimum parameters for the compression strength of porous SS316L	136
4.32	The confirmation result of porous SS316L compression strength	137
4.33	Comparison between the S/N ratio of porous SS316L compression strength before and after optimisation	137
4.34	Average pore size of porous SS316L	145

LIST OF FIGURES

FIGURE NO.	TITLE	PAGE
1.1	Elastic modulus of currently used materials for biomedical application	4
2.1	Graphical definition of biomedical materials, biomaterials and biological biomaterials.	10
2.2	Microstructure of natural bone at (a) inner region of bone, (b) within the wall of macropores and (c) in the cortical bone.	11
2.3	Microstructure of cancellous trabecular bone.	11
2.4	The structure of cortical and trabecular bone.	11
2.5	The structure of cortical and trabecular bone for the healthy and low bone mass	12
2.6	Microstructure of (left) a closed cell foam and (right) an open and interconnected cell foam.	14
2.7	Example of open and interconnected cell foam, indicating some of the typical features.	14
2.8	Bone ingrowth into the pores of porous implant providing a stable and strong bonding or fixation.	15
2.9	Porous hip implants	16
2.10	Young Modulus vs strength of different materials.	18
2.11	Classification of fabrication method for metal foam.	22
2.12	Microstructure of (a) PU foam template and (b) human cancellous bone	23
2.13	Schematic representation of the three-step replication process.	24
2.14	The stainless steel family of alloys.	29

2.15	The binary Fe-Cr phase diagram	30
2.16	Stainless steel implants of (a) The Harrington rod, (b) Total hip replacement.	31
2.17	Schaeffler phase diagram	32
2.18	SEM images of the 17-4 PH stainless steel foams	33
2.19	SEM images of SS316L foams added with a) 15 wt.% $(\text{NH}_4)_2\text{CO}_3$, b) 15 wt.% NH_5CO_3 , c) 30 wt.% $(\text{NH}_4)_2\text{CO}_3$ and d) 30 wt.% NH_5CO_3	33
2.20	Microstructures of porous 316L stainless steel prepared by using the water leaching and sintering methods.	34
2.21	SEM images of the stainless steel 316L sheet foam microstructure produced by the foaming slurry method.	34
2.22	SEM images of the porous 316L stainless steel prepared by SLM observed from different angles	35
2.23	Microstructure of the porous SS316L prepared by the space holder method.	35
2.24	The schematic of sintering mechanism.	37
2.25	Effects of relative sintering neck's diameter on the mechanical properties of porous titanium.	39
2.26	Variation of compressive strength and elongation of $\text{Al-Al}_2\text{O}_3$ due to sintering time and temperature.	40
2.27	Compressive strength and elastic moduli of Ti foam samples sintered at 800°C, 900°C and 1000°C.	40
2.28	Effects of sintering temperature and sintering time on the mechanical properties of porous Cr-Si-Ni-Mo steel	41
2.29	Effect of sintering temperature on the porosity of 316L stainless steel.	42
2.30	Effects of heating rate on the ceramic foams porosity and compressive strength	44
3.1	(a) SEM image of as received SS316L powder, and optical images of (b) PEG, and (c) CMC	53
3.2	(a) Stainless steel SS316L slurry and milling balls in the milling bowl, and (b) and (c) planetary ball mill	56
3.3	Mechanical stirrer	56

3.4	(a) Polyurethane (PU) Foam, and (b) PU foam after slurry impregnation	57
3.5	Tube furnace used for sintering	57
3.6	Vacuum furnace for sintering	58
3.7	Flowchart of the replication method to produce stainless steel SS316L foam	59
3.8	Sintering profile for the preparation of porous stainless steel SS316L	60
3.9	Linseis Thermobalance Thermal Gravimetric Analysis	62
3.10	JEOL JSM6380LA Scanning Electron Microscope	63
3.11	Mitler Toledo density kit used to measure samples density.	65
3.12	Schematic illustration of test specimen	66
3.13	Typical stress-strain diagram	66
3.14	Servopulser UTM testing machine by Shimadzu used for compression fatigue testing.	67
3.15	biological thermostat	68
3.16	P-Diagram porous SS316L preparation	74
4.1	Weight losses versus temperature for the thermal degradation of PEG, CMC and PU foam	78
4.2	Microstructure of porous SS316L produced in the 2nd trial with the materials composition of 4 wt% CMC, 4 wt% PEG, 26 wt% SS316L, 66 wt% H ₂ O and the EDX analysis result.	80
4.3	Microstructure of porous SS316L produced in the 4th trial with the materials composition of 3 wt% CMC, 3 wt% PEG, 30 wt% SS316L, 64 wt% H ₂ O and the EDX analysis result	80
4.4	Digital camera images of (a) SS316L coated PU foam before sintering, (b) sintered 40 wt% SS316L foam, (c) sintered 50 wt. % SS316L foam, and (d) sintered 60 wt. % SS316L foam produced in the fifth trial	81
4.5	Shrinkage percentage of porous stainless steel 316L at different SS316L composition.	81
4.6	Microstructure of the struts for (a) 40 wt% SS316L foam, (b) 50 wt% SS316L foam, and (c) 60 wt% SS316L foam produced in the fifth trial	84

4.7	The shrinkage percentage of porous SS316L with different SS316L composition.	85
4.8	Microstructure of the struts for (a) 60 wt% SS316L foam, (b) 65 wt% SS316L foam, and (c) 70 wt% SS316L foam produced in the sixth trial	86
4.9	Microstructure of the sintered 60 wt% SS316L foam	87
4.10	The shrinkage percentages of stainless steel foam sintered at 1200°C, 1250°C and 1300°C	89
4.11	Density and porosity percentage of porous stainless steel 316L at different SS316L composition produced in the fifth trial	92
4.12	Density and porosity percentage of porous stainless steel 316L at different SS316L composition produced in the sixth trial	93
4.13	Porous SS316L with 70 wt% SS316L composition collapsed after sintering due to incomplete covering of SS316L slurry at the innermost part of PU foam during impregnation process.	94
4.14	Compressive stress strain curve for porous stainless steel with 60 wt% SS316L	94
4.15	Yield strength and elastic modulus of porous SS316L sintered at different temperature	95
4.16	SEM and EDX result after soaked in the SBF for (a) 0 day, (b) 3 days, (c) 7 days and (d) 14 days	100
4.17	S/N and Mean Response Tables and Graphs of Shrinkage Percentage for Porous SS316L Prepared by Ball Milling Method	108
4.18	S/N and Mean Response Tables and Graphs of Shrinkage Percentage for Porous SS316L Prepared by Mechanical Stirring Method	109
4.19	S/N and Mean Response Tables and Graphs of Apparent Density for porous SS316L prepared by Ball Milling Method	114

4.20	S/N and Mean Response Tables and Graphs of Apparent Density for porous SS316L prepared by Mechanical Stirring Method	115
4.21	S/N and Mean Response Tables and Graphs of Total Porosity for porous SS316L prepared by Ball Milling Method	120
4.22	S/N and Mean Response Tables and Graphs of Total Porosity for porous SS316L prepared by Mechanical Stirring Method	121
4.23	S/N and Mean Response Tables and Graphs of Modulus of Elasticity for porous SS316L prepared by Ball Milling Method	126
4.24	S/N and Mean Response Tables and Graphs of Modulus of Elasticity for porous SS316L prepared by Mechanical Stirring Method	127
4.25	S/N and Mean Response Tables and Graphs of Yield Strength for porous SS316L prepared by Ball Milling Method	132
4.26	S/N and Mean Response Tables and Graphs of Yield Strength for porous SS316L prepared by Mechanical Stirring Method	133
4.27	S/N and Mean Response Tables and Graphs of Compression Strength for porous SS316L prepared by Ball Milling Method	138
4.28	S/N and Mean Response Tables and Graphs of Compression Strength for porous SS316L prepared by Mechanical Stirring Method	139
4.29	Microstructure of porous SS316L sintered at 1300 °C and prepared by the ball milling method with different sintering time, cooling and heating rates, and SS316L composition	141

4.30	Microstructure of porous SS316L sintered at 1250 °C and prepared by the ball milling method with different sintering time, cooling and heating rates, and SS316L composition	142
4.31	Microstructure of porous SS316L sintered at 1200 °C and prepared by the ball milling method with different sintering time, cooling and heating rates, and SS316L composition	143
4.32	The struts microstructure of porous SS316L sintered at 1200°C, 1250°C, and 300°C.	144
4.33	Microstructure of porous SS316L sintered at 1200°C, 1250°C and 1300°C at 500× magnification	144



LIST OF ABBREVIATION

ASTM	-	American Society for Testing and Materials
CMC	-	carboxymethyl cellulose
Cps	-	Centipoise
DF	-	Degrees of freedom
DIN	-	German Institute for Standardisation
DOE	-	Design of experiments
ECHC	-	European Commission on Health and Consumers
EDX	-	Energy Dispersive X-Ray
FDA	-	U.S Food and Drug Administration
GPa	-	Gigapascal
ISO	-	International Organization for Standardization
MPa	-	Megapascal
MPIF	-	Metal Powder Industries Federation
SEM	-	Scanning electron microscope
SS316L	-	Stainless steel 316L
PEG	-	Polyethylene glycol
PM	-	Powder Metallurgy
PU	-	Polyurethane
PVA	-	Polyvinyl Alcohol
SBF	-	Simulated Body Fluid
S/N	-	Signal to Noise Ratio
TGA	-	Thermal gravimetric analysis
UTS	-	Ultimate tensile stress
WHO	-	World Health Organization
wt%	-	Weight percentage
SLM	-	Selective Laser Method

LIST OF SYMBOLS

a	-	samples width
b	-	samples length
c	-	samples height
A1	-	1°C/min (Cooling Rate)
A2	-	5°C/min (Cooling Rate)
B1	-	1200°C (Sintering Temperature)
B2	-	1250°C (Sintering Temperature)
B3	-	1300°C (Sintering Temperature)
C1	-	0.5 °C/min (Heating Rate)
C2	-	1 °C/min (Heating Rate)
C3	-	2 °C/min (Heating Rate)
D1	-	60 minutes (Sintering Time)
D2	-	90 minutes (Sintering Time)
D3	-	120 minutes (Sintering Time)
E1	-	60 wt. % SS316L (SS316L composition)
E2	-	65 wt. % SS316L (SS316L composition)
E3	-	70 wt.% SS316L (SS316L composition)
E	-	Modulus of elasticity
σ_c	-	Compression Strength
σ_y	-	Yield Strength
σ	-	Stress
ε	-	Strain
ρ	-	Density
H ₂ O	-	Water
V	-	Volume

W_{dry}	-	dry weight
W_{sub}	-	submerged weight
W_{wet}	-	wet weight



LIST OF APPENDICES

APPENDIX	TITLE	PAGE
A	Microstructure of porous SS316L prepared by foam replication method	168
B	Optical images of porous SS316L after sintering	172



PTTA UTHM
PERPUSTAKAAN TUNKU TUN AMINAH

CHAPTER 1

INTRODUCTION

1.1 Research Background

The mechanical failure of the human body can often be repaired by the surgical implantation of synthetic replacement parts called biological implants. Numerous researches have been conducted over time by the clinicians and engineers to study the physical and mechanical properties of all types of human bones and implants to treat various injuries involving bone replacement. The success of bone replacement with implant depends on many factors such as physical and mechanical properties of the implant material, biocompatibility between a human body with the implant material, patient's health condition and expertise of the surgeon who performs the surgery. At present, the implant material is only able to survive and work well within the human body for about 12 to 15 years. This condition causes re-surgery is needed to monitor the condition of the implant, the patient's health and to replace the implant. Re-surgery and replacement of the implants will involve additional cost to the patient. The cause of the failure of an implant is varies, including the mechanical, chemical, biocompatibility, implant design, surgery, tribology and so forth [1].

Since 1940s, experts from various fields including science, engineering, and medicine have introduced several new processing methods, design concepts, and surgical techniques. Although the 20th century saw many inventions and advances in the development of biomaterials with its own characteristics, however, to date, there is still no implant material that exactly matches the composition, structure, and

property of any part of the human body. In addition, in recent years, nanotechnology, biomimetic, and tissue engineering concepts have rapidly developed and became a new boundary in the development of nanoscale biomaterials [2].

The use of metals as biomedical implants primarily stainless steel, Co-based alloys, Ti and its alloys to replace damaged or failed tissue has begun since the early 1900s. Stainless steel is the first metal implant used successfully in the field of surgery. However, the elastic modulus of stainless steel and Co-Cr alloys is higher than that of the natural bone which is about ten times larger, resulting in some complications of mechanical instability and the structure between the implants and host tissues. The elastic modulus of Ti and its alloy is found to be about five times larger than the natural bone. If a stiffer implant is inserted into hard tissues (eg, Bones), the bones will undergo a reduced mechanical stress which gradually leads to bone absorption. Therefore, this phenomenon is known as a "stress shielding effect" that leads to the death of bone cells [3]. Therefore, low stiffness cellular metals have been produced to overcome this problem.

In the 1970s, the use of porous materials with open pore structure as bone implant has been introduced. Accordingly, this open pore structure promotes the integration of both bones and blood vessels and overcomes the large elastic modulus difference between the bones and the implants. Additionally, porous metals are able to reach similar strength with cancellous bone because of this porous structure. Thus, porous metals have attracted significant attention among medical researchers all over the world due to these unique properties [4].

In order to replace the cancellous bone, there are basically some features that need to be fulfilled by the metal implants which include of having interconnected pores about 30-90% with a pore size in the range of 100-600 μm to provide space for cell migration and new tissue in-growth, and a low Young modulus that similar to the cancellous bone, $<3 \text{ GPa}$ [5].

1.2 Problem Statement

There are two types of orthopedic implants which are temporary implant and permanent implant. Plates and screws are examples of the temporary implant. While for a permanent implant, it usually involved with knees, shoulders, spine, hips, fingers and feet replacements. In the case of a permanent implant, it is very important to ensure that the bonding between the implant material and the living tissue is strong enough and safe. This strong bonding can be achieved through the tissue in-growth within the open and interconnected pores of the implant materials [6]. However, the current metal implant still has some weaknesses. First, the bonding strength is still not high enough and needs to be improved. Second, the large difference of elastic modulus between the bone and implant should be reduced.

Figure 1.1 shows the elastic modulus of most materials that currently used for biomedical applications. From this diagram, it is clearly shows that the elastic modulus of cancellous and cortical bone is very low compared to the elastic modulus of metal implants, especially in the case of stainless steel. This will cause stress shielding to occur on the interface that will affect the long-term stability of the implant [7]. This stress shielding problem still remains as an issue of attention among researchers around the world. In fact, the use of porous materials as implant materials also attracts researchers' interest and attention as a very effective method to reduce excessive stiffness and modulus of elasticity to achieve long-term stability. The elastic modulus of porous metal implants can be modified to match the human bone and thus help prevent the effect of stress shielding on the bones and implants. In addition, porous metal can provide space for bone ingrowth to achieve biological fixation.

REFERENCES

1. Manivasagam, G. Biomedical implants: Corrosion and its prevention—a review. *Recent Patents on Corrosion Science*. 2010.2(i):40–54.
2. Seeram Ramakrishna, Murugan Ramalingam, T .S. Sampath Kumar, W. O. S. Biomaterials: A Nano Approach. *Materials and Manufacturing Processes*. 2014.29(11-12): 1510-1511.
3. Leel J, Leel J, Kim M, Hyun S. Fabrication of Porous Titanium with Directional Pores for Biomedical Applications. 2013.54(2):137-142.
4. Quadbeck, P. Kummel, K. and Hauser, R. Structural and Material Design of Open-Cell Powder Metallurgical Foams. *Advanced Engineering Materials*. 2011.13(11):1024–1030.
5. Cachinho, S. C. P. and Correia, R. N. Titanium porous scaffolds from precursor powders: rheological optimization of TiH₂ slurries. *Powder Technology*.2007. 178(2):109–113.
6. Ryan, G., Pandit, A. and Apatsidis, D. P. Fabrication methods of porous metals for use in orthopaedic applications. *Biomaterials* .2006.27(13):2651–2670.
7. Stephani, G., Quadbeck, P. and Andersen, O. New multifunctional lightweight materials based on cellular metals – manufacturing, properties and applications. *Journal of Physics: Conference Series*.2009.165:012061.
8. Li, Y. Yang, C. Zhao, H. Qu, S. Li, Z. and Li, Y. New developments of Ti-based alloys for biomedical applications. *Materials*.2014.7(3):1709–1800.
9. Kato K, Yamamoto A, Ochiai S, et al. Cytocompatibility and mechanical properties of novel porous 316L stainless steel. *Materials Science and Engineering C*. 2013. 33(5):2736-2743.
10. Dopico-González C, New AM, Browne M. Probabilistic finite element analysis of the uncemented hip replacement-effect of femur characteristics and implant design geometry. *Journal of biomechanics*. 2010.43(3):512-520.
11. Khan, W., Muntimadugu, E., Jaffe, M. and Domb, A. J. Focal Controlled Drug Delivery. *Advances in Delivery Science and Technology*.2014.33–59.
12. Chen, Q. and Thouas, G. A. Metallic implant biomaterials. *Materials Science and Engineering R: Reports*. 2015. 87:1–57.
13. Lu WW, Zhao F, Luk KDK, et al. Controllable porosity hydroxyapatite ceramics as spine cage: fabrication and properties evaluation. *Journal of*

- materials science. Materials in medicine*. 2003.14(12):1039-104614.
14. Polo-Corrales, L., Latorre-Esteves, M. and Ramirez-Vick, J. E. Scaffold design for bone regeneration. *Journal of nanoscience and nanotechnology* .2014.14: 15–56.
 15. Muthutantri, A., Huang, J. and Edirisinghe, M. Novel preparation of graded porous structures for medical engineering. *Journal of the Royal Society Interface the Royal Society* .2008. 5:1459–67.
 16. Fu, Q., Rahaman, M. N., Sonny Bal, B., Brown, R. F. and Day, D. E. Mechanical and in vitro performance of 13-93 bioactive glass scaffolds prepared by a polymer foam replication technique. *Acta Biomaterialia* .2008.4: 1854–1864.
 17. Liu Y, Bao C, Wismeijer D, Wu G. The physicochemical/biological properties of porous tantalum and the potential surface modification techniques to improve its clinical application in dental implantology. *Materials Science and Engineering C*. 2015.49(14):323-329.
 18. Wang, X. *et al.* Topological design and additive manufacturing of porous metals for bone scaffolds and orthopaedic implants: A review. *Biomaterials*.2016. 83: 127–141.
 19. Zerin, I. Bone Generating Fibre Polyhydroxybutyrate (PHB). *Textilefocus.com* Available at: <http://textilefocus.com/2861-2/>.
 20. Čapek, J. *et al.* Highly porous, low elastic modulus 316L stainless steel scaffold prepared by selective laser melting. *Materials Science and Engineering: C*.2016. 69:631–639.
 21. Sola, A., Bellucci, D. and Cannillo, V. Functionally graded materials for orthopedic applications - an update on design and manufacturing. *Biotechnology Advances*. 2016. 34(5):504–531.
 22. Goodall, R. Porous metals: foams and sponges. In: Chang, I. and Zhao, Y. *Advances in Powder Metallurgy*. Cambridge, UK: Woodhead Publishing Limited. 273-307;2013.
 23. Mour, M. *et al.* Advances in porous biomaterials for dental and orthopaedic applications. *Materials*.2010.3(5):2947–2974.
 24. Bellucci, D., Sola, A. and Cannillo, V. A Revised Replication Method for Bioceramic Scaffolds. *Bioceramics Development and Applications* .2011.1:1–8.

25. Udenni Gunathilake, T. M. S., Ching, Y. C., Ching, K. Y., Chuah, C. H. and Abdullah, L. C. Biomedical and microbiological applications of bio-based porous materials: A review. *Polymers* .2017.9(5):1–16.
26. Kennedy, A. Porous metals and metal foams made from powders. In:Kondoh, K. *Powder Metallurgy* . www.intechopen.com. 31-46; 2012.
27. Quadbeck, P., Stephani, G., Kümmel, K., Adler, J. and Standke, G. Synthesis and properties of open-celled metal foams. in *Materials Science Forum* .2007. 534–536:1005–1008.
28. Sampath, U. G. T. M., Ching, Y. C., Chuah, C. H., Sabariah, J. J. and Lin, P. C. Fabrication of porous materials from natural/synthetic biopolymers and their composites. *Materials* .2016. 9(12):1–32.
29. Hsu, H. C., Wu, S. C., Hsu, S. K., Chang, T. Y. and Ho, W. F. Effect of ball milling on properties of porous Ti-7.5Mo alloy for biomedical applications. *Journal of Alloys and Compounds*.2014.582:793–801.
30. Nouri, A., Hodgson, P. and Wen, C. Biomimetic porous titanium scaffolds for orthopedic and dental applications. In: Mukherjee, A. *Biomimetics Learning from Nature*. www.intechopen.com. 415–451;2010.
31. Kokubo, T. and Takadama, H. How useful is SBF in predicting in vivo bone bioactivity? *Biomaterials* .2006. 27: 2907–2915.
32. Drouet, C. Apatite formation: Why it may not work as planned, and how to conclusively identify apatite compounds. *BioMed Research International* .2013. 2013:12.
33. Sharifnabi, A., Fathi, M. H., Yekta, B. E. and Hossainipour, M. Applied Surface Science The structural and bio-corrosion barrier performance of Mg-substituted fluorapatite coating on 316L stainless steel human body implant. *Applied Surface Science*.2014.288:331–340.
34. *Orthopedics, A. Your Hip Surgery*. Available from : <<http://www.associatedorthopaedics.com/associatedorthopedics/jointreplacement-yourhipsurgery.htm>> [5 November 2015]
35. Britton, J. R., Lyons, C. G. and Prendergast, P. J. Measurement of the relative motion between an implant and bone under cyclic loading. *Strain*.2004.40(4): 193–202.
36. Fu, Q., Saiz, E., Rahaman, M. N. & Tomsia, A. P. Bioactive glass scaffolds for bone tissue engineering: state of the art and future perspectives. *Materials*

- Science and Engineering C* .2011.31(7):1245–1256.
37. Bansiddhi, A, Sargeant, T. D., Stupp, S. I. & Dunand, D. C. Porous NiTi for bone implants: a review. *Acta biomaterialia* .2008. 4(4):773–82.
 38. Singh, R. and Dahotre, N. B. Corrosion degradation and prevention by surface modification of biometallic materials. *Journal of materials science. Materials in medicine* .2007.18(5):725–51.
 39. Navarro, M., Michiardi, A, Castaño, O. and Planell, J. A. Biomaterials in orthopaedics. *Journal of the Royal Society, Interface / the Royal Society* . 2008. 5(27): 1137–58.
 40. Jiang, B. et al. A novel method for making open cell aluminum foams by powder sintering process. *Materials Letters* .2005.59(26):3333–3336.
 41. Xie, F., He, X., Lu, X., Cao, S. and Qu, X. Preparation and properties of porous Ti–10Mo alloy by selective laser sintering. *Materials Science and Engineering: C* .2013.33(3):1085–1090.
 42. Kränzlin, N. and Niederberger, M. Controlled fabrication of porous metals from the nanometer to the macroscopic scale. *Materials Horizons* .2015.2(4):359–377.
 43. Tange, M., Manonukul, A. and Srikudvien, P. The effects of organic template and thickening agent on structure and mechanical properties of titanium foam fabricated by replica impregnation method. *Materials Science and Engineering A* .2015. 641:54–61.
 44. Fey, T., Betke, U., Rannabauer, S. and Scheffler, M. Reticulated Replica Ceramic Foams: Processing, Functionalization, and Characterization. *Advanced Engineering Materials*. 2017.1700369:1–15.
 45. Studart, A. R., Gonzenbach, U. T., Tervoort, E. and Gauckler, L. J. Processing routes to macroporous ceramics: A review. *Journal of the American Ceramic Society* .2006.89:1771–1789.
 46. Bairo, F., Novajra, G. & Vitale-Brovarone, C. Bioceramics and Scaffolds: A Winning Combination for Tissue Engineering. *Frontiers in bioengineering and biotechnology* .2015.3:1-17.
 47. Matos, M. J., Dias, S. and Oliveira, F. A. C. Macrostructural changes of polymer replicated open cell cordierite based foams upon sintering. *Advances in Applied Ceramics* .2007.106: 209–215.

48. Amirjan, M. and Khorsand, H. Processing and properties of Al-based powder suspension/slurry: A comparison study of aqueous binder systems, stability and film uniformity. *Powder Technology* .2014. 254:12–21.
49. Hsu, H. C., Hsu, S. K., Wua, S. C., Wang, P. H. and Ho, W. F. Design and characterization of highly porous titanium foams with bioactive surface sintering in air. *Journal of Alloys and Compounds* .2013.575: 326–332.
50. Lee, J.H., Kim, H.E., Shin, K.H. and Koh, Y.H. Improving the strength and biocompatibility of porous titanium scaffolds by creating elongated pores coated with a bioactive, nanoporous TiO₂ layer. *Materials Letters* .2010.64(22): 2526–2529.
51. Suryanarayana, C. and Al-Aqeeli, N. Mechanically alloyed nanocomposites. *Progress in Materials Science* .2013.58(4):383–502.
52. Gotor, F. J., Achimovicova, M., Real, C. and Balaz, P. Influence of the milling parameters on the mechanical work intensity in planetary mills. *Powder Technology* .2013.233:1–7.
53. Kim, J. *et al.* A comparative study of the physical and mechanical properties of porous hydroxyapatite scaffolds fabricated by solid freeform fabrication and polymer replication method. *International Journal of Precision Engineering and Manufacturing*.2011.12(4):695–701.
54. Tiainen, H., Wiedmer, D. and Haugen, H. J. Processing of highly porous TiO₂ bone scaffolds with improved compressive strength. *Journal of the European Ceramic Society* .2013.33(1):15–24.
55. S. Ahmad, N. Muhamad, A. Muchtar, J. Sahari, K. R. Jamaludin, M. H. I. Ibrahim, N. H. M. N. and I. M. Producing of titanium foam using titanium alloy (Al₃Ti) by slurry method. *Proceedings of International Conference in Engineering and Technology (BICET)*. Institut Teknologi Brunei .2008:1–8.
56. Sharifi, H., Divandari, M., Khavandi, A. and Idris, M. Effect of Al powder and silica sol on the structure and mechanical properties of Al₂O₃-ZrO₂ foams. *Acta Metall Sin. (Engl. lett)* .2010.23(4): 241–247.
57. Chen, Q., Mohn, D. and Stark, W. J. Optimization of Bioglass® scaffold fabrication process. *Journal of the American Ceramic Society* .2011.94(12): 4184–4190.
58. Wang, C. *et al.* An improved polymeric sponge replication method for

- biomedical porous titanium scaffolds. *Materials Science and Engineering: C* 2017.70(2):1192–1199.
59. Ho, N. S. K., Li, P., Raghavan, S. and Li, T. The effect of slurry composition on the microstructure and mechanical properties of open-cell Inconel foams manufactured by the slurry coating technique. *Materials Science and Engineering: A* .2017.687(January):123–130.
 60. Beddoes, J. and Parr, J. G. Introduction to Stainless. Third Edition. Materials Park, Ohio: ASM International. 2000.
 61. Al-Mangour, B. Powder Metallurgy of Stainless Steel: State-of-the Art, Challenges, and Development. In: Pramanik, A. and Basak, A.K. *Stainless Steel* .Nova Science Publishers.37-80;2015.
 62. Disegi, J. A. and Eschbach, L. Stainless steel in bone surgery. *Injury* **31**, (2000).
 63. Godbole, N. Yadav, S. and Ramachandran, M. A Review on Surface Treatment of Stainless Steel Orthopedic Implants. *International Journal of Pharmaceutical Sciences Review and Research*. 2016. 36(1):190–194.
 64. Feng, Y. *et al.* Keyhole gas tungsten arc welding of AISI 316L stainless steel. *Materials and Design*.2015. 85(3):24–31.
 65. Talha, M., Behera, C. K. and Sinha, O. P. A review on nickel-free nitrogen containing austenitic stainless steels for biomedical applications. *Materials Science and Engineering C* .2013.33(7):3563–3575.
 66. Mondal, D. P., Jain, H., Das, S. and Jha, A. K. Stainless steel foams made through powder metallurgy route using NH_4HCO_3 as space holder. *Materials and Design* .2015.88:430–437.
 67. Lewis, G. Properties of open-cell porous metals and alloys for orthopaedic applications. *Journal of Materials Science: Materials in Medicine*. 2013.24(10): 2293–2325.
 68. Mutlu, I. and Oktay, E. Mechanical properties of sinter-hardened Cr–Si–Ni–Mo based steel foam. *Materials & Design* .2013.33(3):1125–1131.
 69. Mutlu, I. and Oktay, E. Characterization of 17-4 PH stainless steel foam for biomedical applications in simulated body fluid and artificial saliva environments. *Materials science & engineering. C, Materials for biological applications* .2013.33(3):1125–31.
 70. Mariotto, S. D. F. F., Guido, V., Yao Cho, L., Soares, C. P. and Cardoso, K. R. Porous stainless steel for biomedical applications. *Materials Research*

- .2011.14(2): 146–154.
71. Bakan, H. I. A novel water leaching and sintering process for manufacturing highly porous stainless steel. *Scripta Materialia* .2006.55(2):203–206.
 72. Mirzaei, M. and Paydar, M. H. A novel process for manufacturing porous 316 L stainless steel with uniform pore distribution. *Materials and Design* .2017.121: 442–449.
 73. Rabiei, A. and Garcia-Avila, M. Effect of various parameters on properties of composite steel foams under variety of loading rates. *Materials Science and Engineering: A*.2013.564: 539–547.
 74. Bekoz, N. and Oktay, E. Mechanical properties of low alloy steel foams: Dependency on porosity and pore size. *Materials Science and Engineering A* .2013.576:82–90.
 75. Yan, C., Hao, L., Hussein, A., Young, P. and Raymont, D. Advanced lightweight 316L stainless steel cellular lattice structures fabricated via selective laser melting. *Materials and Design* .2014.55:533–541.
 76. Wakai, F. and Bordia, R. K. Microstructural evolution and anisotropic shrinkage in constrained sintering and sinter forging. *Journal of the American Ceramic Society* .2012.95:2389–2397.
 77. Hermawan, H., Dubé, D. and Mantovani, D. Developments in metallic biodegradable stents. *Acta biomaterialia* .2010.6(5):1693–7.
 78. Kruszewski, K. M. *et al.* Reducing Staphylococcus aureus biofilm formation on stainless steel 316L using functionalized self-assembled monolayers. *Materials Science and Engineering: C* .2013.33(4):2059–2069.
 79. Upadhyaya, G.S *Sintered metallic and ceramic materials: preparation, properties, and applications*.New York: Wiley.150-160; 2000.
 80. Ji, C. H., Loh, N. H., Khor, K. A. and Tor, S. B. Sintering study of 316L stainless steel metal injection molding parts using Taguchi method: final density. *Materials Science and Engineering: A* .2001.311(1-2):74–82.
 81. Zou, C., Liu, Y., Yang, X., Wang, H. and Wei, Z. Effect of sintering neck on compressive mechanical properties of porous titanium. *Transactions of Nonferrous Metals Society of China* .2012.22:485–490.
 82. Rahimian, M., Ehsani, N., Parvin, N. and Baharvandi, H. R. The effect of particle size, sintering temperature and sintering time on the properties of Al–Al₂O₃ composites, made by powder metallurgy. *Journal of Materials*

- Processing Technology* .2009.209(14):5387–5393.
83. Dudek, A. and Włodarczyk, R. Effect of sintering atmosphere on properties of porous stainless steel for biomedical applications. *Materials science & engineering. C, Materials for biological applications* .2013.33(1):434–439.
 84. Xie, F., He, X., Cao, S. and Qu, X. Structural and mechanical characteristics of porous 316L stainless steel fabricated by indirect selective laser sintering. *Journal of Materials Processing Technology* .2013.213(6):838–843.
 85. Tian, H. and Ma, Q. Effects of heating rate on the structure and properties of SiOC ceramic foams derived from silicone resin. *Ceramics International* .2012.38(3):2101–2104.
 86. Gómez, S. Y. *et al.* Relationship between Rheological Behaviour and Final Structure of AlO and YSZ Foams Produced by Replica. *Advances in Materials Science and Engineering* .2012.2012: 1–9.
 87. Kovářík, T. *et al.* Synthesis of open-cell ceramic foam derived from geopolymer precursor via replica technique. *Materials Letters* .2017.209:497–500.
 88. Ehterami, A., Kazemi, M., Nazari, B., Saraeian, P. and Azami, M. Fabrication and characterization of highly porous barium titanate based scaffold coated by Gel/HA nanocomposite with high piezoelectric coefficient for bone tissue engineering applications. *Journal of the Mechanical Behavior of Biomedical Materials* .2018.79(Nov 2017):195–202.
 89. Dewidar, M. M., Khalil, K. A. and Lim, J. K. Processing and mechanical properties of porous 316L stainless steel for biomedical applications. *Transactions of Nonferrous Metals Society of China* .2007.17(1):468–473.
 90. Melorose, J., Perroy, R. and Careas, S. Transfer of manufacturing process for stainless-steel foam to industrial scale. *Statewide Agricultural Land Use Baseline*.2015.2015 1:2–6.
 91. Shimizu, T., Matsuzaki, K., Nagai, H. and Kanetake, N. Production of high porosity metal foams using EPS beads as space holders. *Materials Science and Engineering: A*.2012. 558:343–348.
 92. Guarino, S., Barletta, M., Pezzola, S. and Vesco, S. Manufacturing of steel foams by Slip Reaction Foam Sintering (SRFS). *Materials and Design* .2012.40:268–275.
 93. Kashef, S. *et al.* Fracture mechanics of stainless steel foams. *Materials Science and Engineering A* .2013.578:115–124.

94. Quadbeck, P., Kümmel, K., Hauser, R. and Standke, G. Open Cell Metal Foams—Application-oriented Structure and Material Selection. *Ifam-Dd.Fraunhofer.De* (1966).
95. Kaya, A. C. and Fleck, C. Deformation behavior of open-cell stainless steel foams. *Materials Science and Engineering: A* .2014.615: 447–456.
96. Szewczyk-nykiel, A. and Nykiel, M. Analysis of the Sintering Process of 316L – Hydroxyapatite Composite Biomaterials. *Technical Transaction Mechanics*. .2015:79-92.
97. Tatt, T. K., Muhamad, N., Muchtar, A., Sulong, A. B. and Cherng, N. M. Influence of sintering parameters on the compressive yield strength of stainless steel foams produced by the space holder method. *Sains Malaysiana* .2016.45: 653–658.
98. Joshi, S. and Gupta, G. K. Synthesis & Characterization of Stainless Steel foam via Powder Metallurgy Taking Acicular Urea as Space Holder. *Material Science Research India* .2015.12:43–49.
99. Pandya, S., Ramakrishna, K. S., Raja Annamalai, A. and Upadhyaya, A. Effect of sintering temperature on the mechanical and electrochemical properties of austenitic stainless steel. *Materials Science and Engineering A* .2012.556: 271–277.
100. Kurgan, N. Effect of porosity and density on the mechanical and microstructural properties of sintered 316L stainless steel implant materials. *Materials & Design* .2014.55: 235–241.
101. Samer, A., German, R. M. and Muhsan, A. S. Effects of Sintering Temperature and Cooling Rate on Mechanical Properties of Powder Injection Molded 316L Stainless Steel. *Solid State Phenomena*.2012.185:1–4.
102. Pachauri, P. and Hamiuddin, M. Optimization of Injection Moulding Process Parameters in MIM for Impact Toughness of Sintered Parts. *Cloud Publications International Journal of Advanced Materials and Metallurgical Engineering* .2015.1:1–11.
103. Chen, D.C. and Chen, C.F. Use of Taguchi method to develop a robust design for the shape rolling of porous sectioned sheet. *Journal of Materials Processing Technology* .2006.177:104–108.
104. Ghani, J. A., Choudhury, I. A. V Hassan, H. H. Application of Taguchi method in the optimization of end milling parameters. *Journal of Materials Processing*

- Technology*.2004.145:84–92.
105. Mustapha, F. *et al.* Preliminary study on the fabrication of aluminium foam through pressure assisted sintering dissolution process. *Journal of Materials Processing Technology* .2010. 210:1598–1612.
 106. Cunningham, E., Dunne, N., Walker, G. and Buchanan, F. High-solid-content hydroxyapatite slurry for the production of bone substitute scaffolds. *Proceedings of the Institution of Mechanical Engineers , Part H: Journal of Engineering in Medicine*. 2009. 223: 727
 107. Li, C. L., Wang, H., Zhou, X. Y., Li, J. and Liu, H. Z. Debinding of stainless steel foam precursor with 3-D open-cell network structure. *Transactions of Nonferrous Metals Society of China (English Edition)* .2010.20:2340–2344.
 108. Klar, E. Samal, PK. Sintering and Corrosion Resistance. *Powder Metallurgy Stainless Steels: Processing, Microstructures, and Properties*. ASM International.2007:60–100.
 109. Zhu, X., Jiang, D., Tan, S. and Zhang, Z. Improvement in the Strut Thickness of Reticulated Porous Ceramics. *Journal of the American Ceramic Society* .2001.84:1654–1656.
 110. Wu, K., Park, H.S. and Willert-Porada, M. Pyrolysis of polyurethane by microwave hybrid heating for the processing of NiCr foams. *Journal of Materials Processing Technology* .2012.212:1481–1487.
 111. Lei, G., German, R. M. and Nayar, H. S. Influence of Sintering Variables on the Corrosion-Resistance of 316L Stainless-Steel. *Powder Metallurgy International* 1983.15:70–76.
 112. Sarkar, S. K. *et al.* Fabrication and Characterization of Porous TCP coated Al₂O₃ Scaffold by Polymeric Sponge Method. *Journal of the Korean Ceramic Society* .2008. 45: 579–583.
 113. Naveed Hosseini, S., Salimi Jazi, H. and Fathi, M. Novel electrophoretic deposited nanostructured forsterite coating on 316L stainless steel implants for biocompatibility improvement. *Materials Letters* .2015. 143:16–19.
 114. Li, Y. *et al.* New Developments of Ti-Based Alloys for Biomedical Applications. *Materials* .2014.2014(7):1709–1800.
 115. Jamaludin, A. R., Kasim, S. R., Abdullah, M. Z. and Ahmad, Z. A. Physical, mechanical, and thermal properties improvement of porous alumina substrate through dip-coating and re-sintering procedures. *Ceramics International* .2015.

- 42: 7717–7729.
116. Kurgan, N. and Varol, R. Mechanical properties of P/M 316L stainless steel materials. *Powder Technology*.2010. 201: 242–247.
 117. Dewidar, M. Influence of processing parameters and sintering atmosphere on the mechanical properties and microstructure of porous 316L stainless steel for possible hard-tissue applications. *International Journal of Mechanical and Mechanics Engineering* . 2012. 12: 10–24.
 118. Seerane, M., Chikwanda, H. and Machaka, R. Determination of Optimum Process for Thermal Debinding and Sintering using Taguchi Method. *Materials Science Forum* .2015. 829: 138–144.
 119. Feng, P. *et al.* Sintering behaviors of porous 316L stainless steel fiber felt. *Journal of Central South University* .2015. 22:793–799.
 120. Torres, Y., Lascano, S., Bris, J., Pavon, J. and Rodriguez, J. A. Development of porous titanium for biomedical applications: A comparison between loose sintering and space-holder techniques. *Materials Science and Engineering C* .2014.37(1):148-155.
 121. International Organization for Standardization Standard (2011). *ISO 13314:2011(E)*. Switzerland:ISO 2011.
 122. Smith, B. H., Szyniszewski, S., Hajjar, J. F., Schafer, B. W. and Arwade, S. R. Steel foam for structures: A review of applications, manufacturing and material properties. *Journal of Constructional Steel Research* .2012.71: 1–10.
 123. Emilie, A.S. *Design And Evaluation Of Novel Open-Pore Titanium Foams*. PhD Thesis. University of Nevada, Reno; 2011.
 124. Purnama, A., Hermawan, H., Couet, J. and Mantovani, D. Assessing the biocompatibility of degradable metallic materials: state-of-the-art and focus on the potential of genetic regulation. *Acta biomaterialia* .2010.6(5):1800–1807.
 125. Taguchi, G. Quality engineering through design optimization. *Kraus International Publications* .1984:1106–1113.
 126. Manonukul, A., Tange, M., Srikudvien, P., Denmud, N. and Wattanapornphan, P. Rheological properties of commercially pure titanium slurry for metallic foam production using replica impregnation method. *Powder Technology* .2014.266:129–134.
 127. Verlee, B., Dormal, T. and Lecomte-Beckers, J. Density and porosity control of sintered 316L stainless steel parts produced by additive manufacturing. *Powder*

- Metallurgy* .2012.55(4): 260–267.
128. Nor, M. A. A. M., Akil, H. M. and Ahmad, Z. A. The effect of polymeric template density and solid loading on the properties of ceramic foam. *Science of Sintering* .2009.41:319–327.
 129. Won, S. *et al.* Fabrication of porous titanium scaffold with controlled porous structure and net-shape using magnesium as spacer. *Materials Science & Engineering C* .2013. 33:2808–2815.
 130. Muthutantri, A., Huang, J. and Edirisinghe, M. Novel method of preparing hydroxyapatite foams. *Journal of Materials Science: Materials in Medicine*.2008. 19:1485–1490.
 131. Gao, Y. *et al.* Novel TiC/Ti Open Cellular Foams Prepared by a Modified Sponge-coating Method Using High Frequency Induction Heating Process. *Journal of Materials Science and Technology* .2013.29:339–343.
 132. Yook, S.W. *et al.* Reverse freeze casting: a new method for fabricating highly porous titanium scaffolds with aligned large pores. *Acta biomaterialia* .2012.8(6):2401–2410.
 133. Ahmad, S., Muhamad, N. and Muchtar, A. Development and Characterization of Titanium Alloy Foams. *International Journal of Mechanical and Materials Engineering (IJMME)* .2010.5: 244–250.
 134. Chen, W., Allen, J. K., Tsui, K.L. and Mistree, F. A Procedure for Robust Design : *Journal of Mechanical Design* .1996.118: 478–485.
 135. Kackar, R. N. Off-line quality control, parameter design, and the Taguchi method. in *Quality Control, Robust Design, and the Taguchi Method* .1989. 76:51–76.
 136. Motz, R. Pippan, B. K. Mechanical properties and determination. in *Handbook of Cellular Metals: Production, Processing, Applications* .WILEY. :183–189.2002.
 137. Nakaş, G. I., Dericioglu, A. F. & Bor, S. Fatigue behavior of TiNi foams processed by the magnesium space holder technique. *Journal of the mechanical behavior of biomedical materials*.2011. 4:2017–23.
 138. Fan, X. *et al.* Bone-like apatite formation on HA/316L stainless steel composite surface in simulated body fluid. *Transactions of Nonferrous Metals Society of China (English Edition)* .2009. 19:347–352.
 139. Mutlu, I. Sinter-coating method for the production of TiN-coated titanium foam

- for biomedical implant applications. *Surface and Coatings Technology* .2013.232:396–402.
140. Li, J., Yang, H., Wang, H. and Ruan, J. Low elastic modulus titanium–nickel scaffolds for bone implants. *Materials Science and Engineering: C* .2014.34:110–4.
 141. Dehaghani, M. T. and Ahmadian, M. Porous vitalium-base nano-composite for bone replacement: Fabrication, mechanical, and in vitro biological properties. *Journal of the Mechanical Behavior of Biomedical Materials*.2016.57:297–309.
 142. Esen, Z. and Bor, Ş. Characterization of Ti–6Al–4V alloy foams synthesized by space holder technique. *Materials Science and Engineering:A*.2011.528: 3200–3209.
 143. Wei, S. *et al.* Effect of Sintering Time on the Microstructure of Porous Tantalum. *Rare Metal Materials and Engineering* .2015.44: 319–322.
 144. Ma, J. *et al.* Effect of ball milling on the rheology and particle characteristics of Fe–50%Ni powder injection molding feedstock. *Journal of Alloys and Compounds* .2014.590:41–45.
 145. Alem, A., Pugh, M. D. and Drew, R. A. L. Open-cell reaction bonded silicon nitride foams: Fabrication and characterization. *Journal of the European Ceramic Society* .2014. 34: 599–609.
 146. Hsu, H.C. *et al.* Processing and mechanical properties of porous Ti–7.5Mo alloy. *Materials & Design* .2013.47:21–26.
 147. Sharma, M., Gupta, G. K., Modi, O. P., Prasad, B. K. and Gupta, A. K. Titanium foam through powder metallurgy route using acicular urea particles as space holder. *Materials Letters*.2011. 65:3199–3201.
 148. Thavornyutikarn, B. *et al.* Porous 45S5 Bioglass®-based scaffolds using stereolithography: Effect of partial pre-sintering on structural and mechanical properties of scaffolds. *Materials Science and Engineering C*.2017.75:1281–1288.
 149. Mediaswanti, K. *et al.* A Review on Bioactive Porous Metallic Biomaterials. *Journal of Biomimetics Biomaterials Tissue Engineering*.2013.18:1–8.
 150. Yan, C. *et al.* Microstructure and mechanical properties of aluminium alloy cellular lattice structures manufactured by direct metal laser sintering. *Materials Science and Engineering A*.2015.628:238–246.
 151. Michailidis, N., Stergioudi, F., Tsouknidas, A. and Pavlidou, E. Compressive

- response of Al-foams produced via a powder sintering process based on a leachable space-holder material. *Materials Science & Engineering A* .2011.528: 1662–1667.
152. Nouri, A., Hodgson, P. D. and Wen, C. E. Effect of process control agent on the porous structure and mechanical properties of a biomedical Ti-Sn-Nb alloy produced by powder metallurgy. *Acta Biomaterialia*.2010.6:1630–1639.
 153. Ravichandran, M. and Anandakrishnan, V. Optimization of powder metallurgy parameters to attain maximum strength coefficient in Al–10 wt% MoO₃ composite. *Journal of Materials Research* .2015.30:2380–2387.
 154. German, R. M. Coarsening in sintering: Grain shape distribution, grain size distribution, and grain growth kinetics in solid-pore systems. *Critical Reviews in Solid State and Materials Sciences*.2010.35:263–305.
 155. German, R. M. Sintering Simplified: Surface Area, Density, and Grain Size Relations. *Materials Science Forum* .2016.835:50–75.
 156. Hannink, G. and Arts, J. J. C. Bioresorbability, porosity and mechanical strength of bone substitutes: What is optimal for bone regeneration? *Injury* .2011.42:S22–S25.
 157. Jung, A. *et al.* Improved Mechanical Properties of Nano- nickel Strengthened Open Cell Metal Foams Nanonickel Coated Aluminum Foam for Enhanced Impact Energy Absorption. *Advanced Engineering Materials*.2011. 13:22-28
 158. Madhani, J., Pendrey, D., Situ, R. and Brown, R. Modification of Porous Alumina Ceramics with Bioinert and Bioactive Glass Coatings. *Advanced Materials Research* .2007.32:211–214.
 159. Zhu, X., Jiang, D. and Tan, S. Improvement in the strength of reticulated porous ceramics by vacuum degassing. *Materials Letters* .2001.51:363–367.
 160. Zhang, L., He, Z. Y., Zhang, Y. Q., Jiang, Y. H. and Zhou, R. Rapidly sintering of interconnected porous Ti-HA biocomposite with high strength and enhanced bioactivity. *Materials Science and Engineering C* .2016.67:104–114.
 161. Kim, B.N., Hiraga, K., Morita, K. and Yoshida, H. Effects of heating rate on microstructure and transparency of spark-plasma-sintered alumina. *Journal of the European Ceramic Society* .2009.29:323–327.
 162. Yang, D. *et al.* Effects of sintering temperature and holding time on porosity and shrinkage of glass tubes. *Ceramics International* .2016.42:5906–5910.
 163. Vivanco, J., Aiyangar, A., Araneda, A. and Ploeg, H. Mechanical

characterization of injection-molded macro porous bioceramic bone scaffolds.

Journal of the Mechanical Behavior of Biomedical Materials .2012.9:137–152.

164. Poly, P. *et al.* Porous Poly(para-phenylene) Scaffolds for Load-Bearing Orthopedic Applications. *Journal of the Mechanical Behavior of Biomedical Materials* .2014.30:347-357.



PTTA UTHM
PERPUSTAKAAN TUNKU TUN AMINAH